## **Research Article**

# Asynchronous Two-Way Ranging Using Tomlinson-Harashima Precoding and UWB Signaling

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This paper demonstrates two methods which simultaneously undertake synchronization and ranging based on a time-of-arrival approach with bidirectional communication to bypass the need for accurate synchronous clocking. In order to alleviate multipath effects, Tomlinson-Harashima precoding and UWB signaling are used to measure the distance between pairs of sensors. The proposed schemes are shown to be effective under certain assumptions and the analysis is supported by simulation and numerical studies.

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#### 1. INTRODUCTION

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In many sensor network applications, it is useful or even required for sensors to be aware of their locations [1–5]. Due to the low-power, lower-cost, and simple configuration requirements of wireless sensor networks, GPS devices, accurate synchronous clocks, and manually configuring location information into each sensor during deployment may be precluded. However, accurate relative location estimates are achievable by relying on precise distance measurements between neighboring sensors [6–13].

Previous work [14] suggests that bidirectional signaling can be used to bypass the use of expensive clocks, but the analysis is limited by the assumption that only the line-ofsight (LOS) path exists. However, in real radio channels, there may exist multiple transmission paths between the sensors. In order to investigate the effect of this multipath interference on the distance estimations, this paper augments the previous schemes by utilizing channel estimation [15, 16], a Tomlinson-Harashima (TH) precoding (the modulo inverse filter [17]), and ultra-wideband (UWB) signaling for distance measurement in static multipath channels based on the time-of-arrival (TOA) methodology. Two distributed solutions are described for distance estimation in ad-hoc sensor networks: (1) asynchronous ranging via TH precoding (ARTHP) and (2) asynchronous ranging via ultra-wideband (ARUWB). For the ARTHP method, channel information and a module inverse filter are used to combat the multipath effect and maximize the correlator output so that the estimator can carry out the range measurement accurately (detailed in Section 2). For the ARUWB method, the two-way UWB communication system is used to provide precise TOA estimates in multipath channels (detailed in Section 3). In this paper, the two proposed solutions integrate time synchronization, information processing, and ranging task to complete joint synchronization and ranging for wireless ad-hoc sensor networks with two-way communications.

Preequalization techniques are used principally in data transmission systems to combat the effect of interference caused by nonideal (multipath) channels. This paper proposes the application of TH precoding to the estimation of distance between pairs of sensors using bidirectional communication links over multipath channels. Assume that the channel characteristics do not vary significantly with time. Therefore, given the channel state information in the transmitter, it is possible to precode the information prior to transmission such that the problems which are generally inherent with the equalization at the receiver, such as the noise enhancement, can be avoided. The key point in TH precoding is the nonlinear modulo-arithmetic operation to guarantee the stability of the precoder.

TH precoding is derived from linear preequalization at the transmitter. Disregarding the modulo congruence, TH precoding transforms the ISI channel H(z) to a memoryless one and the system overall behavior is well approximated by the AWGN model. In [18, 19] a new precoding technique, called flexible precoding (FLP) or distribution-preserving precoding, is proposed. Unlike TH precoding, FLP resembles linear equalization at the receiver. The disadvantage of linear equalization is that noise is filtered with 1/H(z) and the desired precoding gain is lost. Compared with FLP, the performance of TH precoding has lower precoding loss and the implementation of TH precoding has simpler circuitry complexity. However, TH recoding requires the channel knowledge, which may limit its usage in randomly time-varying wireless channels. To avoid this drawback, a feedback channel, which continuously updates the channel state information, may be applied. These feedback channels are usually available in standardized wireless communication systems.

For TH precoding, the following are three possible scenarios. In the first, the transmitter and receiver share the same incorrect channel state information. In the second, the receiver has perfect channel knowledge but the transmitter has an incorrect channel estimate. In the third, channel state information is only available at the transmitter. In this work, given a pair of sensors, sensor A, and sensor B, the third scenario is considered where sensor B estimates the channel using a training sequence sent by sensor A, inverts the channel impulse response, and then sends the preequalized signal back to sensor A. This allows sensor A to accurately estimate the distance. Current literature on ranging using preequalization techniques for wireless sensor networks is limited. Related work in different precoding scenarios can be found in [20–26] and the references therein.

Besides the preequalization technique, a two-way TOAbased ranging technique with UWB signaling is proposed and the performance on ranging in UWB systems is studied. UWB radiolocation functionality usually relies on the ability to perform precise estimates of the TOA. Different TOA estimation methods for UWB propagation signals are investigated in [27–32]. Notice that the above research on ranging in UWB systems focuses on simulation and measurements of UWB ranging and positioning or on theoretical accuracy of UWB synchronization and ranging for UWB signals with no specific application IEEE 802.15.3a/4a [33-35] signal formats. On the other hand, the CRLBs for several UWB signal formats are derived to complement the previous literature on UWB ranging by providing a theoretical framework for the analysis of achievable ranging accuracy [36]. In addition, a global distributed solution is proposed to enable the simultaneous performance of time synchronization and positioning in UWB ad-hoc networks [37]. It is demonstrated that a cooperative and distributed maximization of the log-likelihood of range estimates can reduce the uncertainty on estimated positions in comparison with classical distributed weighted least squares approaches. However, the analysis in [36] is impractical since it does not take the effect of clock parameters into account. In [37], although the described solution considers the clock-dependent ranging error, the operation of the proposed synchronization scheme and the diffusion algorithm that ensures the convergence of clock parameters are complex for ad-hoc networks.

In general, ranging accuracy depends on precise time synchronization, time stamp reading, and information management such as computation and signal processing. This paper presents an estimation-theoretic analysis of the proposed measurement mechanisms to assess the achievable estimation accuracy. Two main ranging errors are considered: (1) the clock-dependent ranging error and (2) the signal-tonoise- (SNR-) dependent ranging error. These two ranging errors are examined carefully to assess their impact on the TOA ranging accuracy.

The rest of the paper is organized as follows. Section 2 describes the ARTHP method and analyzes the ranging accuracy. Section 3 presents the ARUWB approach and assesses the estimation accuracy for both AWGN and multipath channels. Then, Section 4 addresses the performance of the proposed ranging approaches and discusses the trade-offs between ARTHP and ARUWB in terms of energy consumption, circuitry and computational complexity, and ranging accuracy. Finally, Section 5 draws conclusions and shows future research directions.

#### 2. ASYNCHRONOUS RANGING VIA TH PRECODING (ARTHP)

This section describes the Asynchronous Ranging via TH Precoding (ARTHP) technology to examine the effect of multipath interference on ranging problems. The proposed method outlines one way to estimate the distance using channel estimation and the notion of cooperation between pairs of wireless sensors. Given two sensors A and B, sensor A initiates communication by sending a training sequence. Then, sensor B carries out a channel estimation based on maximizing the output of the correlator. Based on channel estimation, sensor B generates a modified training sequence for correlating with the training sequence sent from sensor A. Once sensor B detects the peak of the correlator output, it triggers a time counter and initiates the TH precoding. After receiving the signal from sensor B, sensor A stops the timer based on the performance of the correlator output and calculates the propagation time  $t_{ab}$ . Thus, sensor B estimates the channel and applies the TH precoding using a training sequence sent by sensor A, and allows A to accurately estimate the distance. The basic principle of the ARTHP method is captured in Figure 1.

- (i) Sensor A sends training sequence s(t) for channel estimation and time synchronization in sensor B.
- (ii) Sensor B carries out a channel estimation based on maximizing the output of the correlator and time synchronization using the time stamps of transmission and reception in sensors A and B.
- (iii) Based on the channel estimation, sensor B generates a modified training sequence  $y_2(t)$  that can be used to



FIGURE 1: The ARTHP method: block diagram of a bidirectional communication and distance measurement system using channel estimation and TH precoding.



FIGURE 2: The correlator structure using channel information.

correlate with the received training sequence  $y_1(t)$  sent from A. The correlator output of sensor B,  $r_B(t)$ , is

$$r_B = \int_0^{MT_c} y_1(t) y_2(t) dt,$$
 (1)

where  $T_c$  represents the time interval between symbols and  $MT_c$  is the correlation time.

- (iv) Once sensor B detects the peak of the correlator output, it triggers a time counter, initiates the TH precoding, and records the processing delay. Then, sensor B transmits the preequalized signal and the delay information back to sensor A.
- (v) After receiving the signal from sensor B, sensor A stops the timer based on the performance of the correlator output and calculates the propagation time  $t_{ab}$ .

This method shows that time delay estimation is possible without synchronous clocking. Based on the system architecture in Figure 1, the following subsections explore the impact of the TH precoding and the correlation procedure on ranging accuracy.

#### 2.1. TH precoding with channel knowledge

Since preequalization and correlator performance play critical roles in the distance measurement, the performance of the TH precoding in sensor B and the correlator output of sensor A are analyzed to help understand the behavior of the method. The precoder structure is shown in Figure 3. The modulo operation  $Q_I(\cdot)$  is defined as  $Q_I(a) = a + b$ , where *b* is the unique integer multiple of *I* for which  $Q_I(a) \in$ (-I/2, I/2]. Assuming that the channel impulse response H(Z) is an *m*th order FIR filter, the approximation of the estimated channel impulse response  $\hat{H}(Z)$  is given by

$$\hat{H}(Z) = \sum_{n=0}^{m-1} \hat{g}_n Z^{-n} \simeq \sum_{n=0}^{m-1} (g_n + \Delta g_n) Z^{-n},$$
(2)

where  $g_n$  and  $\hat{g}_n$  are the coefficients of channel impulse response H(Z) and estimated channel impulse response  $\hat{H}(Z)$ , respectively. Note that the difference  $\Delta g_n$  between  $g_n$  and  $\hat{g}_n$  depends on channel estimation errors.

According to Figure 3, the output of the modulo operation  $X_k(Z)$  in sensor B is

$$X_{k}(Z) = S_{k}(Z) + X_{k}(Z)(1 - \hat{H}(Z)) - l_{k}I$$
  
=  $\frac{S_{k}(Z) - l_{k}I}{\hat{H}(Z)}$ , (3)

where  $l_k$  is an integer. Therefore, the received signal  $P_k(Z)$  in sensor A is

$$P_{k}(Z) = X_{k}(Z)H(Z) + N_{k}(Z)$$

$$= (S_{k}(Z) - l_{k}I) \cdot \frac{H(Z)}{\hat{H}(Z)} + N_{k}(Z)$$

$$= (S_{k}(Z) - l_{k}I) \cdot \frac{\sum_{n=0}^{m-1} g_{n}Z^{-n}}{\sum_{n=0}^{m-1} \hat{g}_{n}Z^{-n}} + N_{k}(Z),$$
(4)

where  $N_k(Z)$  is the received noise.

As a result of modulo reduction and providing that the magnitude of the input data and *I* are chosen such that  $\hat{S}_k(Z) \simeq P_k(Z)$ , the data output is

$$\widehat{S}_k(Z) \simeq P_k(Z) \pmod{I}$$
 (5)

$$\simeq S_k(Z) \cdot \frac{\sum_{n=0}^{m-1} g_n Z^{-n}}{\sum_{n=0}^{m-1} \hat{g}_n Z^{-n}} + N'_k(Z) \tag{6}$$

$$= S_k(Z) \cdot \sum_{n=0}^{\infty} c_n Z^{-n} + N'_k(Z),$$
(7)

where

$$c_n = \begin{cases} \frac{g_0}{\hat{g}_0}, & n = 0\\ \frac{(g_n - \sum_{j=1}^n \hat{g}_j c_{n-j})}{\hat{g}_0}, & n \ge 1. \end{cases}$$
(8)

Note that the coefficient  $c_n$  can be shown to be bounded in terms of the estimation errors using mathematical induction. Hence, there exists an upper bound  $\delta$  for tap gain errors caused by channel estimation errors and an upper bound *B* for  $c_n$  ( $n \ge 1$ ), which is multiple of  $\delta/|\hat{g}_0|$ .

By optimal  $L_2$  finite impulse response (FIR) approximation [39], a discrete infinite impulse response (IIR) which is analytic in { $|z| > \rho$ ,  $\rho < 1$ } (i.e., possessing a power series in  $Z^{-1}$  convergent on the unit circle),

$$F(Z) = \sum_{n=0}^{\infty} f_n Z^{-n} \tag{9}$$

with  $f_n = c_n$ , can be approximated by a discrete *q*-coefficient finite impulse response (denoted by FIR(*q*))

$$\hat{F}(Z) = \sum_{n=0}^{q-1} \hat{f}_n Z^{-n},$$
(10)

where  $\hat{f}_n = c_n$ .

Given a high SNR and small channel estimation errors, the coefficient  $c_0$  in (8) is approaching one such that the signal term is dominant in (7). Therefore, the noise may be assumed to be negligible in this case. Therefore, based on (10), the data output  $\hat{S}_k(Z)$  can be further approximated by

$$\widehat{S}_k(Z) = S_k(Z) \cdot \sum_{n=0}^{q-1} c_n Z^{-n}.$$
(11)

Then the correlator output of sensor A,  $r_A$ , is given by

$$r_{A} = \int_{0}^{MT_{c}} \sum_{n=0}^{q-1} c_{n} s(t - nT_{c}) s(t) dt$$
  
=  $MT_{c} + \sum_{n=1}^{q-1} c_{n} \int_{0}^{MT_{c}} s(t - nT_{c}) s(t) dt$  (12)  
=  $MT_{c} + \sum_{n=1}^{q-1} c_{n} R_{A}^{n}$ ,

where

$$R_{A}^{n} = \int_{0}^{MT_{c}} s(t - nT_{c})s(t)dt.$$
(13)

From the derivation in [40–43], the distribution of  $R_A^n$  is given by

$$R_A^n \sim \mathcal{N}\left(0, MT_c\left(1-2\left|\varepsilon_n\right|+2\varepsilon_n^2\right)\right), \tag{14}$$

where  $\varepsilon_n = (\Delta \tau/T_c) \pm N_{\varepsilon}T_c$  denotes the normalized fractional timing offset between the two training sequences for the *n*th component. Note that  $N_{\varepsilon_n}$  is the smallest integer such that  $\varepsilon_n \in (-1, 1)$ . Therefore, given the channel information, the distribution of  $r_A$  is

$$r_A \sim \mathcal{N}\left(\mu_{r_A}, \sigma_{r_A}^2\right),\tag{15}$$

where  $\mu_{r_A} = MT_c$  and  $\sigma_{r_A}^2 = \sum_{n=1}^{q-1} c_n^2 MT_c (1-2|\varepsilon_n|+2\varepsilon_n^2)$ . Hence, as channel estimation errors approach zero (i.e.,  $B, \delta \rightarrow 0$ ), we have

$$\lim_{B,\delta\to 0} r_A = MT_c. \tag{16}$$

With the TH precoding in sensor B, the correlator output  $r_A$  converges to  $MT_c$  when the channel estimation errors approach zero. On the other hand, without precoding in sensor B, the distribution of  $r_A$  can be expressed by the same form as in (15) with  $c_n = g_n$ . Clearly, the precoding greatly reduces the variance in the correlator output.

#### 2.2. Analysis of ranging accuracy

The fundamental limitation on the ranging accuracy of the estimates is related to the form of the signal and the clock, including signal bandwidth, signal-to-noise ratio (SNR), and timing calibration. Assume that the random range error and range bias error from propagation conditions are negligible. The range-measurement accuracy may be characterized by the measurement error

$$\sigma_R = \left(\sigma_S^2 + \sigma_{\rm clock}^2\right)^{1/2},\tag{17}$$

where  $\sigma_s$  is the SNR-dependent random ranging accuracy and  $\sigma_{clock}$  is the clock-dependent random ranging accuracy. Note that  $\sigma_s$  relates the accuracy of synchronous distance estimates to the signal-to-noise ratio and the effective bandwidth of the signal. The expression of  $\sigma_{clock}$  is the added inaccuracy due to the asynchronous clocking mechanism.



FIGURE 3: Tomlinson-Harashima precoding and linearized description.

#### 2.2.1. Clock-dependent ranging accuracy

Suppose that sensors A and B are equipped with clocks that are asynchronous in both frequency and phase. The random variable T denotes the sensor estimate of the true t; thus  $T_{ab}$ is an estimate of the true time  $t_{ab}$  and  $T_i^A$  is an estimate of the time  $t_i^a$  as measured by the clock of sensor A. From Figure 1, the estimated transmission time is

$$T_{ab} = \frac{T_5^A - T_{del}^A - T_1^A - T_{obs}^A}{2},$$
 (18)

where  $T_{del}^A = Z \cdot T_{del}^B$ ,  $T_{del}^B = T_{pro}^B + T_{obs}^B$ , and  $Z = (T_1^A - T_0^A)/(T_3^B - T_2^B)$ . Note that all measurements  $T_i^A$  and  $T_j^B$  are assumed to be independent normal random variables with the same variance  $\sigma^2$  caused by the measurement error in the clock. This normality assumption is justified in [44] when the clock skew is small. Z is a scale factor that represents how much faster or slower clock A moves than clock B;  $T_{obs}^A$  and  $T_{obs}^B$  are the estimated observation time of the correlators in sensors A and B with distributions  $\mathcal{N}(t_{obs}^A, \sigma_{T_{obs}}^2)$  and  $\mathcal{N}(t_{obs}^B, \sigma_{T_{obs}}^2)$ , respectively;  $T_{pro}^B$  is the estimated processing time of the TH precoder in sensor B with distribution  $\mathcal{N}(t_{obs}^B, \sigma_{T_{obs}}^2)$ . Since  $\sigma_{T_{obs}}^2$ ,  $\sigma_{T_{obs}}^2$ , and  $\sigma_{T_{pro}}^2$  as the variance  $2\sigma^2$ . Thus, the distribution of the estimated delay time  $T_{del}^B$  is given by  $T_{del}^B \sim \mathcal{N}(\mu_{T_{del}}^B, \sigma_{T_{del}}^2)$ , where  $\mu_{T_{del}^B} = t_{pro}^B + t_{obs}^B = t_{del}^B$  and  $\sigma_{T_{del}^B}^2 = \sigma_{T_{pro}}^2 + \sigma_{T_{obs}}^2 = 4\sigma^2$ . Since the measurement errors are small, which are the proper conditions for the Gaussian approximation derived in [45–47], the distribution of  $T_{del}^A$  is

$$T_{\rm del}^A \sim \mathcal{N}\left(\mu_Z \mu_{T_{\rm del}^B}, 4\mu_Z^2 \sigma^2 + t_{\rm del}^{B^{-2}} \sigma_Z^2\right). \tag{19}$$

Therefore, the distribution of  $T_{ab}$  can be sensibly approximated by

$$T_{ab} \sim \mathcal{N}\left(\mu_{T_{ab}}, \sigma_{T_{ab}}^2\right),\tag{20}$$

where  $\mu_{T_{ab}} = (1/2)(t_5^A - \mu_Z t_{del}^B - t_1^A - t_{obs}^A)$  and  $\sigma_{T_{ab}}^2 = (1/4)[(4+4\mu_Z^2)\sigma^2 + t_{del}^B \sigma_Z^2]$ . Thus, the clock-dependent ranging accuracy  $\sigma_{clock}$  is given by

$$\sigma_{\rm clock}^2 = \sigma_{D_{ab}}^2 = c^2 \sigma_{T_{ab}}^2. \tag{21}$$

#### 2.2.2. SNR-dependent ranging accuracy

The SNR-dependent ranging accuracy of the distance measurement is influenced by the error sources such as channel estimation, correlator performance, and signal format. Due to channel estimation errors, sensor B may possess erroneous channel information, which may degrade the performance of the TH precoder. Since the operation of the ARTHP method is complex, in this paper the channel estimation is assumed to be accurate (i.e., the variance of the correlator is negligible and the proper correlation peak is chosen) such that the analysis of the proposed approach can be simplified. In this case, the communication channel reduces to an AWGN channel with direct path only. Accordingly, the accuracy of synchronous distance estimates [48–50] is related to the signalto-noise ratio, the distance, and the effective bandwidth of the signal, which is given by

$$\sigma_{S} \ge \frac{c \cdot d_{ab}}{2\beta_{e} \sqrt{2\text{SNR}}},\tag{22}$$

where  $\beta_e$  is the effective bandwidth of the signal [50]. Hence, from (21) and (22), the estimation error is

$$\sigma_R = \left(\sigma_S^2 + \sigma_{\text{clock}}^2\right)^{1/2} \ge \sqrt{\frac{c^2 d_{ab}^2}{8\beta_e^2 \text{SNR}} + c^2 \sigma_{T_{ab}}^2}.$$
 (23)

#### 3. ASYNCHRONOUS RANGING VIA UWB

An alternative approach is to use a two-way TOA-based ranging technique with UWB signaling. In standard UWB systems, the preamble of a packet can be used to achieve time synchronization. Considering the cooperation between a pair of sensors, in the ARUWB protocol, time calibration is carried out by bidirectional communication without using preamble patterns to compensate the phase and frequency of a clock.

Suppose that sensors A and B are equipped with clocks (oscillators) that are assumed to be asynchronous in both frequency and phase. Denote  $t_i^a$  and  $t_j^b$  as the time stamps in sensors A and B, respectively; let  $t_{del}^a$  and  $t_{del}^b$  be the delay time in sensors A and B, respectively;  $t_{ab}$  is the signal propagation time. The estimation of the ARUWB method proceeds as shown in Figure 4.

- (i) Sensor A transmits a message, which is a ranging sequence comprising K symbols and containing the times  $t_0^a$  and  $t_1^a$  (the times indicated on its clock at the start and the end of the transmission, resp.).
- (ii) Sensor B receives the first symbol at time  $t_2^b$  (which is  $t_{ab}$  seconds after it is transmitted) and receives the last symbol at time  $t_3^b$ .



FIGURE 4: The ARUWB method: sensor A receives its reply at  $t_5^a$ ; this is equal to  $t_1^a + 2t_{ab} + t_{del}^a$ , from which A can estimate  $t_{ab}$  and hence the distance; in this variation, sensor B can calculate the difference between its clock  $(t_3^b - t_2^b)$  and A's clock using the time-stamped information in A's messages  $(t_1^a - t_0^a)$ .

- (iii) Sensor B calibrates its clock to A's using the differences  $t_1^a t_0^a$  (which is known from A's message) and  $t_3^b t_2^b$  (the arrival times).
- (iv) Some time  $t_{del}$  later, sensor B transmits the time  $t_{del}^a = z \cdot t_{del}^b$  that has elapsed since reception of A's message along with the time stamp  $t_4^b$  (the time on B's clock when it transmits). These times are adjusted (if necessary) using the scale factor  $z = (t_1^a t_0^a)/(t_2^b t_2^b)$ .
- (v) Sensor A receives the reply from sensor B when its clock reads  $t_5^a$  (the time indicated on its clock at the start of the reception). The transmission time  $t_{ab}$  can be calculated as

$$t_{ab} = \frac{t_5^a - t_1^a - t_{del}^a}{2}.$$
 (24)

Notice that the clock calibration is achieved by transmitting a ranging sequence using bidirectional UWB links. Based on the estimation procedures, the ranging performance is analyzed considering clock-dependent estimation accuracy and SNR-dependent estimation accuracy for both AWGN and multipath channels in the following subsections.

#### 3.1. ARUWB in AWGN channels

#### 3.1.1. Clock-dependent ranging accuracy

Referring to Figure 4 and using a Gaussian approximation (which is justified in [45-47]), the distribution of the estimated distance  $D_{ab}$  can be well approximated by

$$D_{ab} \sim N(\mu_{D_{ab}}, \sigma_{D_{ab}}^2) \tag{25}$$

with  $\mu_{D_{ab}} = c \cdot \mu_{T_{ab}} = d_{ab}$  and  $\sigma_{D_{ab}}^2 = c^2 \sigma_{T_{ab}}^2 = (c^2/4)[(2 + 2\mu_Z^2)\sigma^2 + t_{del}^b \sigma_Z^2]$ , where *c* is the propagation speed of the signal;  $\sigma$  is the timing resolution;  $\mu_Z$  and  $\sigma_Z^2$  are the mean and variance of the random variable *Z*, respectively;  $\mu_{T_{ab}}$  and  $\sigma_{T_{ab}}^2$ 

are the mean and variance of the random variable, the transmission time  $T_{ab}$ , respectively. Note that the mean of random variable  $D_{ab}$  is the true value of the distance between sensors A and B and the variance of  $D_{ab}$  depends on the variance of the timing measurement  $\sigma$ , the characteristic of the clockadjustment factor Z, and the time delay  $t_{del}^b$ .

Therefore, the clock-dependent ranging accuracy  $\sigma_{clock}$  is given by

$$\sigma_{\rm clock}^2 = \sigma_{D_{ab}}^2 = c^2 \sigma_{T_{ab}}^2, \tag{26}$$

which is derived as in (25).

#### 3.1.2. SNR-dependent ranging accuracy

For ranging applications using UWB signals, in this work the CRLB for UWB signal formats derived in [36] are used to assess the SNR-dependent ranging accuracy. Given a distance  $d_{ab}$  and a channel transfer function, the synchronous ranging accuracy is given by

$$\sigma_{S} \geq \frac{c}{4\pi} \sqrt{\frac{N_{0}}{2T \int_{f_{L}}^{f_{H}} f^{2} \left| H(f, d_{ab}) \right|^{2} \text{PSD}_{\text{MASK}}(f) df}}, \quad (27)$$

with channel transfer function

$$H(f, d_{ab}) = \alpha_0(\tau_0, d_{ab})e^{j2\pi f \tau_0},$$
(28)

where  $\alpha_0(\tau_0, d_{ab})$  is the attenuation factor, which depends on both distance and propagation delay and may be determined based on channel characteristics; *T* is the transmission time;  $[f_L, f_H]$  is frequency range of the signal;  $PSD_{MASK}(f)$  is the power emission mask. Note that in this paper  $PSD_{MASK}(f)$  is assumed to be a constant equal to  $G_0 = -41.3$  dbm/MHz as regulated by the FCC [36].

For the purpose of comparison, an ideal channel with a transfer function independent of frequency and dependent



FIGURE 5: The distributions of correlator outputs of sensor A with/without TH precoding (15) with the timing offset  $\Delta \tau = 0.5T_c$ ,  $MT_c = 0.5$ , and q = 10 (left); the distribution of distance measurement in multipath channels using TH precoding (23) with a timing resolution of 1 ns (right top) and 0.1 nanosecond (right bottom): q = 10,  $t_{ab} = 10^{-7}$ ,  $t_4^b = 3$ ,  $t_{obs}^b = 2$ ,  $t_{obs}^b = 0.2$ ,  $t_2^b = 1.25$ ,  $t_1^a = 0.75$ , and  $t_0^a = 0.25$  second.

upon distance between transmitter and receiver as the inverse of the square of distance  $d_{ab}$  is considered to evaluate the sensitivity of the ranging performance to the multipath effect. Equation (22) therefore can be further expressed as

$$\sigma_{S} \ge \frac{c \cdot d_{ab}}{4\pi} \sqrt{\frac{3N_{0}}{2TG_{0}(f_{H}^{3} - f_{L}^{3})}}$$
(29)

with the effective bandwidth of the signal

$$\beta_e = \sqrt{\frac{3}{4\pi^2 T (f_H^3 - f_L^3)}},$$
(30)

where *T* is equal to  $(t_1^a - t_0^a)$ ,  $N_0 = 2.935 \times 10^{-11}$  W/Hz,  $G_0 = 7.413 \times 10^{-14}$  W/Hz, and  $f_H$  and  $f_L$  are the highest and lowest frequency of UWB frequency bands, respectively. Note that the ranging accuracy in different UWB signal formats are related to the difference in bandwidth and the center frequency.

Thus, for an ideal channel, the estimation error  $\sigma_R$ , given by the root-sum-square of the error components, is

$$\sigma_{R} = \left(\sigma_{S}^{2} + \sigma_{\text{clock}}^{2}\right)^{1/2} \ge \sqrt{\frac{3N_{0}c^{2}d_{ab}^{2}}{32\pi^{2}TG_{0}\left(f_{H}^{3} - f_{L}^{3}\right)}} + c^{2}\sigma_{T_{ab}}^{2}.$$
(31)

#### 3.2. ARUWB in multipath channels

#### 3.2.1. Clock-dependent ranging accuracy

In multipath channels, the time stamp of the received signal is determined by the timing resolution and the propagation delay. Applying the Gaussian approximation, the distribution of the estimated distance  $D_{ab}$  is

$$D_{ab} \sim N(\mu_{D_{ab}}, \sigma_{D_{ab}}^2) \tag{32}$$

with  $\mu_{D_{ab}} = c \cdot (\mu_{T_{ab}} + \tau_l) = d_{ab} + c\tau_l$  and  $\sigma_{D_{ab}}^2 = c^2 \sigma_{T_{ab}}^2 = (c^2/4)[(2+2\mu_Z^2)\sigma^2 + t_{del}^{b^{-2}}\sigma_Z^2]$ , where  $\tau_l$  is the propagation delay of the *l*th multipath component. Again the clock-dependent ranging accuracy  $\sigma_{clock}$  is

$$\sigma_{\text{clock}}^2 = \sigma_{D_{ab}}^2 = c^2 \sigma_{T_{ab}}^2. \tag{33}$$

Observe that when the LOS path is significantly attenuated, the distance measurement might be biased by an incorrect choice of multipath component as derived in (32). On the other hand, given a signal with a large SNR and bandwidth in an environment with a dominant LOS path and moderate multipath, the estimated propagation time may be unbiased with a correct choice of the signal arrival time such that the clock-dependent ranging accuracy in multipath channels is close to that in AWGN channels. Thus, the above analysis suggests that in a strong multipath environment, the clock-dependent ranging accuracy might be dominated by the multipath effect instead of the timing resolution as in AWGN channels.

#### 3.2.2. SNR-dependent ranging accuracy

Based on (27), the synchronous ranging accuracy can be further derived as

$$\sigma_{S} \geq \frac{c \cdot d_{ab}}{4\pi} \sqrt{\frac{3N_{0}}{2TG_{0}(f_{H}^{3} - f_{L}^{3})}} \cdot \eta, \qquad (34)$$



FIGURE 6: The synchronous ranging accuracy of the ARUWB method with fixed observation time T = 1.83 microseconds and varying distance  $d_{ab}$  (from the first perspective) in ideal and AWGN channels (29) (left) and a multipath channel with a dominant LOS path (34) (right).



FIGURE 7: The synchronous ranging accuracy of the ARUWB method with fixed distance  $d_{ab} = 30$  m and varying SNR (from the second perspective) in ideal and AWGN channels (29) (left) and a multipath channel with a dominant LOS path (34) (right).



FIGURE 8: The distribution of asynchronous distance measurement using the ARUWB method with a timing resolution of 0.1 nanosecond:  $t_{ab} = 10^{-7}$ ,  $t_4^b = 0.3 + 2.92 \,\mu s$ ,  $t_5^b = 0.3 + 1.92 \,\mu s$ ,  $t_2^b = 0.3$ ,  $t_1^a = 0.25 + 1.83 \,\mu s$ , and  $t_0^a = 0.25$ , in ideal and AWGN channels (31) (left) and a multipath channel with a dominant LOS path (37) (right).

where

$$\eta = \frac{1}{d_{ab}} \cdot \sqrt{\frac{\int_{f_L}^{f_H} f^2 \operatorname{PSD}_{MASK}(f) df}{\int_{f_L}^{f_H} f^2 |H(f, d_{ab})|^2 \operatorname{PSD}_{MASK}(f) df}}$$
(35)

with channel transfer function

$$H(f, d_{ab}) = \sum_{k=0}^{N-1} \alpha_k(\tau_k, d_{ab}) e^{j2\pi f \tau_k}.$$
 (36)

Observe that the first term in (34) is the SNR-dependent ranging accuracy in an ideal channel and the second term  $\eta$  can be considered as the performance loss due to the multipath effect, which is examined via numerical studies in Section 4.

From (33) and (34), the measurement error  $\sigma_R$  can be expressed as follows:

$$\sigma_{R} = \left(\sigma_{S}^{2} + \sigma_{\text{clock}}^{2}\right)^{1/2} \ge \sqrt{\frac{3N_{0}c^{2}d_{ab}^{2}}{32\pi^{2}TG_{0}\left(f_{H}^{3} - f_{L}^{3}\right)}} \cdot \eta^{2} + c^{2}\sigma_{T_{ab}}^{2}.$$
(37)

#### 4. SIMULATION AND NUMERICAL RESULTS

This section demonstrates the performance of the proposed distance measurement algorithms. Assume that the propagation time is  $t_{ab} = 10^{-7}$  s (i.e., the true distance is  $d_{ab} = 30$  m) for all distance measurement settings.

The first set of experiments evaluates the performance of the distance measurement using channel estimation with TH precoding. Note that the choice of the  $\{t_i^a, t_j^b\}$  values is purely arbitrary in order to show that the proposed technique is able to joint synchronization and ranging with two-way communications. Figure 5(left) depicts the corresponding correlator output of sensor A. Observe that the correlator output  $r_A$ without pre-equalization may have larger variance than with TH precoding due to the multipath effects.

Assume the transmitted waveform is a simple rectangular pulse with a zero phase characteristic,

$$a(t) = \operatorname{rect}\left(\frac{t}{t_p}\right),\tag{38}$$

where  $t_p$  is the pulse width. In our case,  $t_p = T_c$ . Figure 5(right) shows the typical performance of the asynchronous bidirectional distance measurement scheme using TH precoding in multipath channels with the parameters detailed in the caption and the clocks providing a resolution based on the symbol rates of the training sequence, 1 Gigasymbol per second (Gsps) (i.e., 1 nanosecond) and 10 Gsps (i.e., 0.1 nanosecond), respectively. Observe that as the distance  $d_{ab} = 30$  m, the  $\sigma_{ab}$  is about 6 cm with a timing resolution 0.1 nanosecond. Note that an accurate clock with complicated hardware is required for distance estimation using a



FIGURE 9: The comparison of the asynchronous distance measurement applying the ARUWB method (using (31) and (37)) with the same settings in Figure 8 and the UWB ranging solution in [37] (using (11) and (17)), in ideal and AWGN channels (left) and a multipath channel with a dominant LOS path (right).

higher symbol rate (higher timing resolution) though providing a higher measurement accuracy.

The second set of experiments examines the performance of the ARUWB method in both AWGN and multipath channels with synchronous clocking. The purpose of these experiments is to explore the influence of multipath effects on the ranging performance. The two-ray ground reflection model with the same parameters used in the ARTHP method is considered to evaluate the corresponding measurement errors. Two perspectives are investigated to compare the ranging accuracy using different UWB signal formats: (1) ranging accuracy with fixed observation time T and varying distance  $d_{ab}$ ; (2) ranging accuracy with fixed distance  $d_{ab}$  and varying observation time T (i.e., with varying SNR). From the first perspective, Figure 6 depicts the synchronous ranging error, which is proportional to the distance between a pair of sensors. Observe that for the UWB signalings, a DS-UWB high-band signal has the best ranging accuracy due to its higher frequency band and larger operation bandwidth and a MB-OFDM Band 1 signal has the worst ranging accuracy because of its lower frequency band and smaller operation bandwidth. As shown in Figure 6, when the distance  $d_{ab}$ is equal to 30 m, the standard deviation  $\sigma_{d_{ab}}$  of a DS-UWB high-band signal is about 1.8 cm, 12 cm, and 30 cm in ideal (left), AWGN (left), and multipath (right) channels, respectively. Therefore, given time synchronization, the ARUWB method with DS-UWB High Band signals may be a good approach for ranging.

From the second perspective and (29), note that the estimation error is dominated by the factor  $T(f_H^3 - f_L^3)$ , which implies that operation frequencies and observation time will determine the estimation accuracy. Given a SNR, MB-OFDM signals have larger observation times compared with DS-UWB signals since the signal energy is given by  $E_s = T \cdot \text{PSD}_{\text{MASK}} \cdot (f_H - f_L)$ . Figure 7 shows that, again, the proposed method using UWB High Band signals with time synchronization may have better ranging performance in both AWGN (left) and multipath (right) channels.

The third set of experiments studies the performance of the ARUWB method in multipath channels with asynchronous clocking. Since the channel experimental parameters highly depend on the measured environment, in this set of experiments the two-ray ground reflection model is chosen. The parameters for the channel configuration are  $\alpha_0 = 0.8$ ,  $\alpha_1 = 0.5$ ,  $\tau_0 = 0$  ns, and  $\tau_1 = 5$  ns. Figure 8 illustrates the impact of time synchronization and multipath effects on the distance measurement. Applying the ARUWB method with a DS-UWB High Band signal and given a timing resolution 0.1 ns, the standard deviation  $\sigma_{d_{ab}}$  of the estimation is about 30 cm, 50 cm, and 80 cm in ideal (left), AWGN (left) and multipath (right) channels, respectively. Note that though a DS-UWB High Band signal has the best



FIGURE 10: The distributions of the distance measurement in a multipath channel with a dominant LOS path using the UWB ranging method in [37, equation (17)], the ARTHP (23), and ARUWB (37) approaches with UWB signaling given the parameters detailed in the captions of Figures 8 and 9.

ranging accuracy in an ideal channel, all of the UWB signal formats have roughly the same estimation performance as shown in Figure 8(left), which implies that the clockdependent ranging error may dominate the ranging measurement under the circumstances of asynchronous clocking in an ideal channel. However, as shown in Figure 8(right), compared with the clock-dependent ranging error, the SNRdependent ranging error may dominate estimation performance in multipath channels due to the performance loss caused by multipath effects.

Figure 9 compares the ARUWB method and a UWB ranging solution [37] in an ideal channel and a multipath channel with a dominant LOS path via bi-directional communications. Given the same settings as detailed in the caption of Figure 8 and based on (31) and (37) in Section 3 and [37, equations (11) and (17)] with  $W_{\text{LOS}} = 0.61$ ,  $W_{G_{\text{LOS}}} = 1$ ,  $W_{E_{\rm LOS}}$  = 0,  $\sigma_{\rm LOS}$  = 0.0068,  $W_{
m NLOS}$  = 0.39,  $W_{G_{
m NLOS}}$  = 1,  $W_{E_{\rm NLOS}} = 0$ , and  $\sigma_{\rm NLOS} = 0.0102$  [38], the performance studies show that the measurement results of these two techniques are very closed. It is important to remark that the existing UWB approach [37] considers clock-dependent errors and multipath effects and uses a probabilistic model to describe the weights of different multipath components such that the ranging performance can be investigated based on the channel scenarios. However, many assumptions are made when analyzing the clock-dependent errors and the descriptions of parameter settings, such as how to obtain the SNR-dependent errors and how to set the weights for dif-

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ferent multipath components, are not clear. In the ARUWB method, the clock-dependent error is studied and time synchronization mechanism is performed. Moreover, based on the framework in [36], the SNR-dependent errors are further derived under different channel scenarios. Considering the clock-dependent and SNR-dependent estimation errors, the proposed UWB method illustrates a sensible way to assess the ranging performance via bi-directional communications.

For the ARTHP and ARUWB methods, although ranging performance seems to be better in the ARTHP method (with channel information), the performance improvement is achieved at the cost of consuming signal resources for obtaining channel knowledge. Hence, a fair comparison of the proposed techniques with and without channel information requires considering longer signal duration and more signal energy for the ARUWB technique (without channel knowledge). As a result, the following evaluation is made given the same energy consumption in each method. Assume the transmission path is symmetric and the radio dissipates  $E_{elec}$  in the transmitter or receiver circuitry and  $E_{\rm pro}$  in the information processing. Based on the estimation procedures in the ARTHP method, the radio expends:  $E_{(ARTHP)} = 6E_{elec(ARTHP)} + 5E_{pro(ARTHP)}$ , including the operations for communication and signal processing such as signal transmission and reception, channel estimation, correlation, TH precoding, and range-measurement calculation. Similarly, for the ARUWB method, the total energy consumption is  $E_{(ARUWB)} = 4E_{elec(ARUWB)} + 2E_{pro(ARUWB)}$ , which is dissipated for signal transmission and reception, timing calibration, and distance estimation. Since computation is much cheaper than communication, we have  $E_{(ARTHP)} \approx$  $6E_{\text{elec}(\text{ARTHP})}$  and  $E_{(\text{ARUWB})} \approx 4E_{\text{elec}(\text{ARUWB})}$ , which may decide the relationship between  $E_{\text{elec}(\text{ARTHP})}$  and  $E_{\text{elec}(\text{ARUWB})}$  for a given energy.

Given the above settings, Figure 10 shows that the performance of the ARTHP method with DS-UWB High Band signals is superior to that of the ARUWB method with different UWB signal formats due to the contributions of multipath to the distance estimations. Note that the ARTHP method does not require any signaling for the ranging task. Compared with the ARUWB method, the system architecture of the ARTHP approach has greater circuitry requirement and computational complexity due to channel estimation and TH precoding. From Figures 6 to 10, observe that under the circumstance of a dominant LOS path, the ARUWB approach may be a good technique for sensor ranging; on the other hand, if the LOS path is attenuated significantly, the ARTHP approach may be preferred since the multipath effect can be canceled out by the preequalization.

#### 5. CONCLUSION

This paper presents two decentralized methods which simultaneously undertake synchronization and ranging based on an asynchronous two-way TOA approach for wireless ad-hoc sensor networks. These asynchronous and cooperative communication procedures may simplify the computational and circuitry complexity of the ranging estimation in each sensor. In order to alleviate the multipath effect, Tomlinson-Harashima precoding and UWB signaling are used for the distance measurement between pairs of sensors. In the ARTHP technique, an algorithm is presented to cancel the channel effect, which is crucial to the ranging accuracy. In the ARUWB method, the range-measurement accuracy highly benefits from the well-known features of UWB signaling such as in communication and radio-location applications to provide precise time-of-arrival estimates in multipath channels. Sensible settings for the ranging problems using the ARTHP and ARUWB approaches are presented and the proposed mechanisms are simulated and analyzed to assess the accuracy of the distance estimation. Depending on the measurement accuracy, the parameters in each technique can be determined to achieve desired performance.

For the two proposed ranging solutions, tradeoffs are found between model complexity, energy consumption, computational complexity, and sensible model description in real systems. Future plans will involve generalizing the methods to consider certain failure scenarios and to explore the sensitivity of the proposed schemes to system models and network operation.

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